

Module 4F2: Nonlinear Systems and Control

Lectures 4–5: Describing Functions

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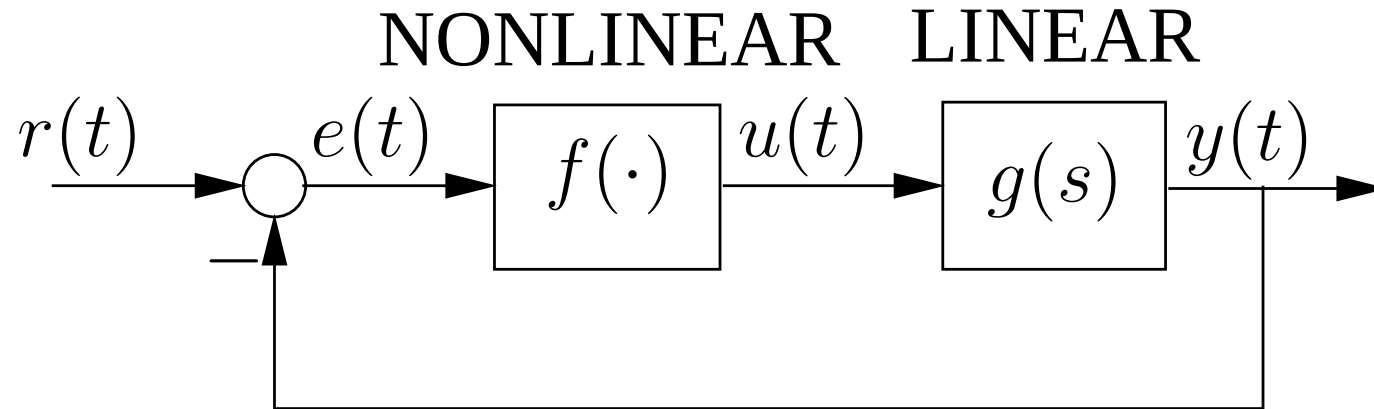


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- Relies on a *low-pass* assumption.
- Generalises Nyquist stability theorem.



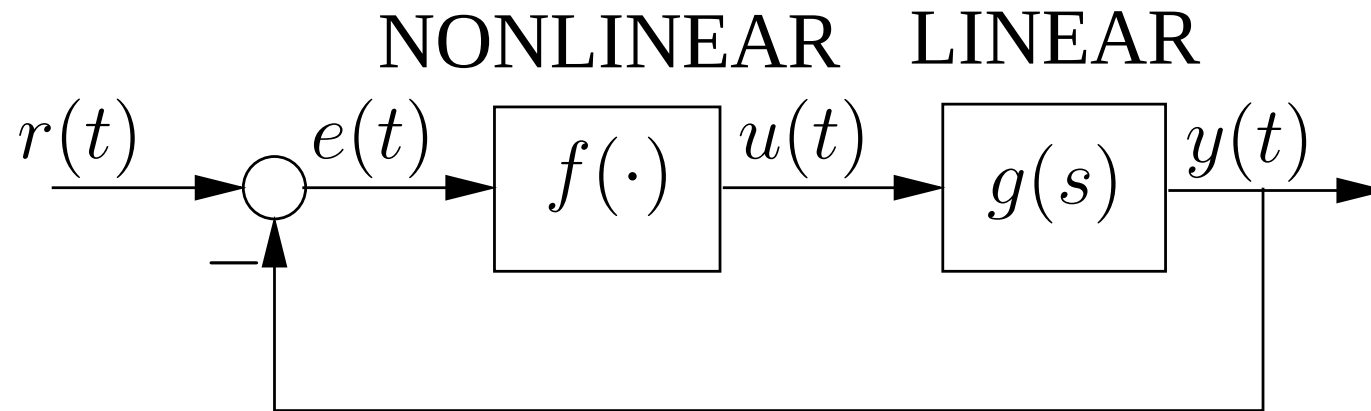
Nonlinear feedback system



- Assume $e(t) = E \sin(\omega t)$, and $r(t) \equiv 0$.



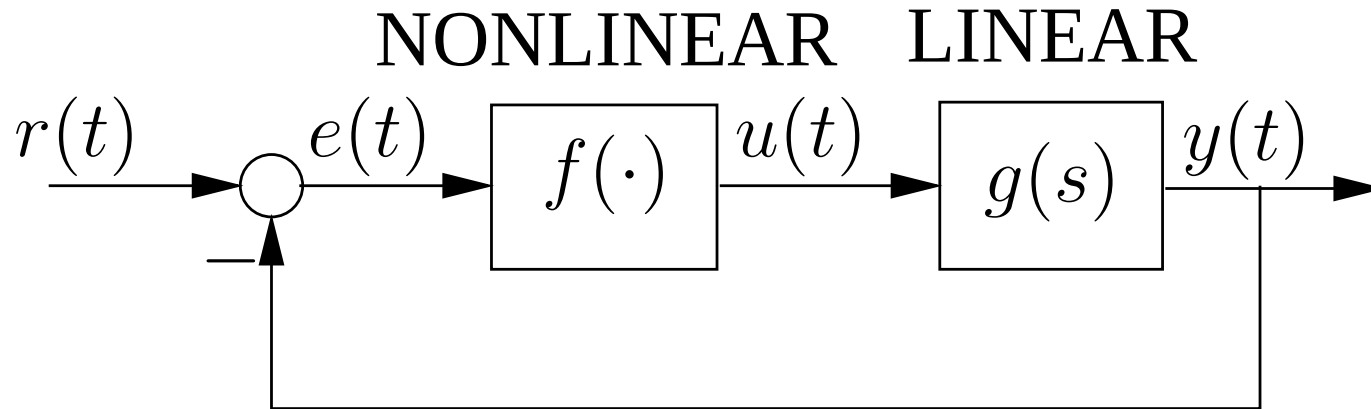
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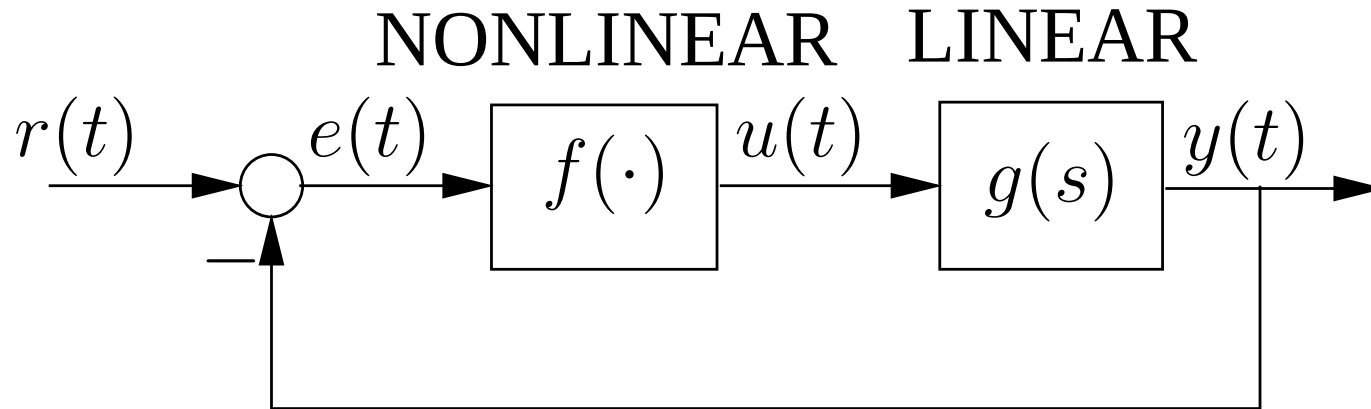
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- Assume $g(s)$ is *low-pass* — $y(t)$ has first harmonic only.
- But $y(t) = -e(t)$ — **harmonic balance**.



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$$V_1 = \frac{1}{\pi} \int_0^{2\pi} f(E \sin \theta) \cos \theta \, d\theta.$$



Harmonic balance

Suppose that

$$u(t) \approx U_1 \sin(\omega t) + V_1 \cos(\omega t) = \text{Im}(U_1 + jV_1)e^{j\omega t}$$



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But

$$0 \equiv y(t) + e(t)$$

$$\Rightarrow 0 \equiv \text{Im}[(g(j\omega)(U_1 + jV_1) + E)e^{j\omega t}] = 0$$

$$\Rightarrow 0 = g(j\omega)(U_1 + jV_1) + E.$$



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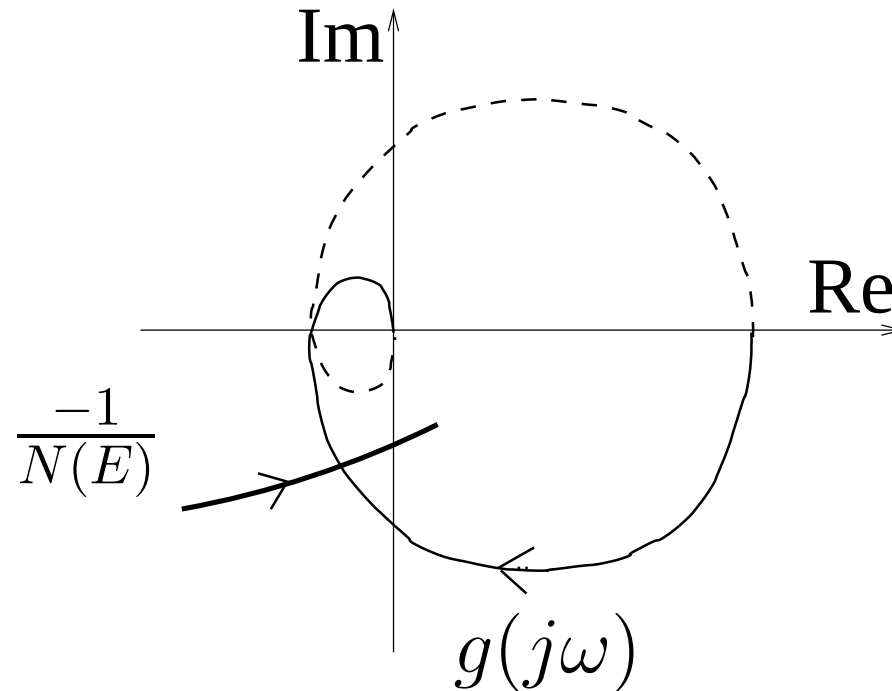
$$g(j\omega) = \frac{-1}{N(E)}.$$

Think of $N(E)$ as *equivalent linear gain*.

Compare with Nyquist: $g(j\omega) = \frac{-1}{k}$.



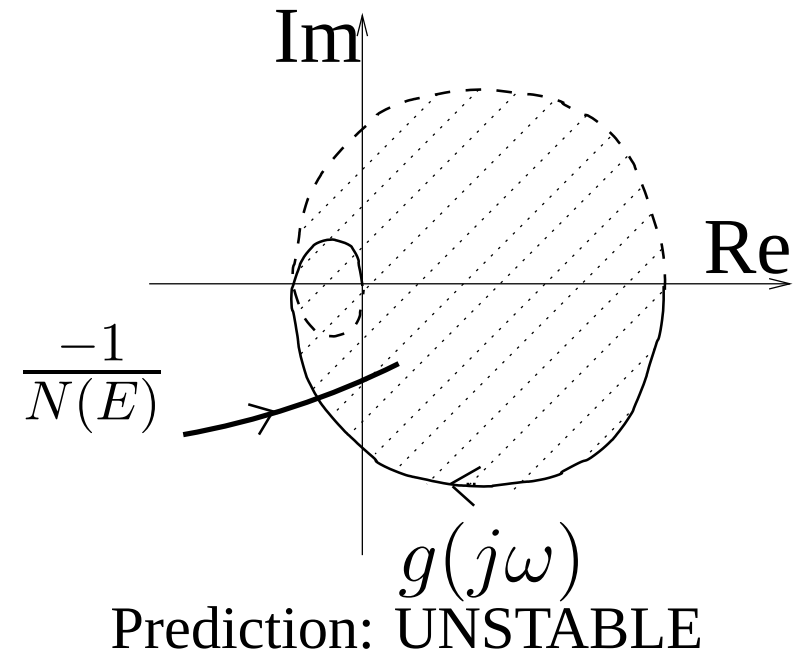
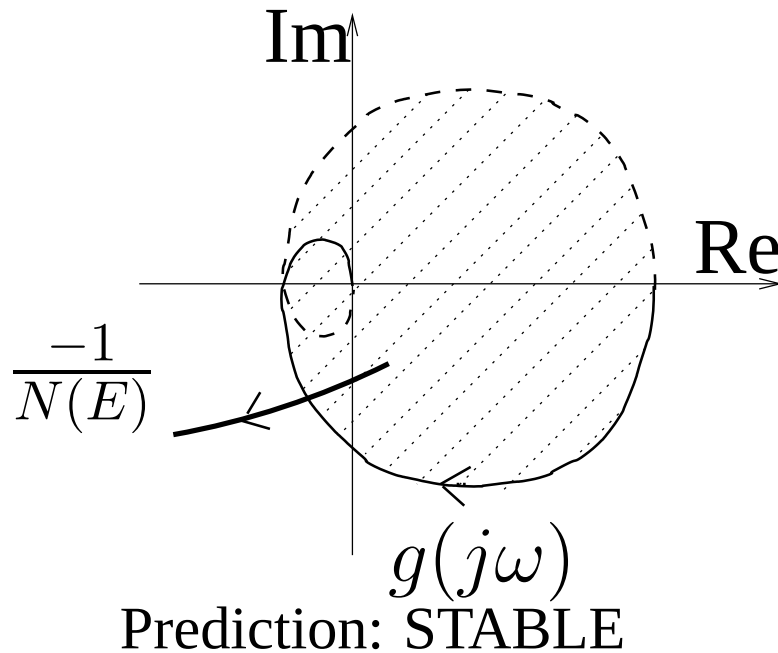
Graphical interpretation



Arrows denote
direction of
increasing ω and
 E



Stability of limit cycle



DF of relay nonlinearity

$$f(e) = \text{sign}(e)$$

$\text{sign}(\sin(\omega t))$ is odd. Hence $V_1 = 0$.

$$\begin{aligned} U_1 &= \frac{1}{\pi} \int_0^{2\pi} \text{sign}(E \sin \theta) \sin \theta \, d\theta, \\ &= \frac{1}{\pi} \int_0^{\pi} \sin \theta \, d\theta - \frac{1}{\pi} \int_{\pi}^{2\pi} \sin \theta \, d\theta \\ &= \frac{4}{\pi}. \end{aligned}$$

Hence

$$N(E) = \frac{4}{\pi E}$$



DF of polynomial nonlinearity

$$f(e) = e^n \quad (n \text{ odd})$$

$$\sin^n \theta = \frac{2}{2^n} \sum_{k=0}^{\frac{n-1}{2}} (-1)^{\left(\frac{n-1}{2}-k\right)} \binom{n}{k} \sin([n - 2k]\theta)$$

Last term, $k = \frac{n-1}{2}$, gives fundamental component.



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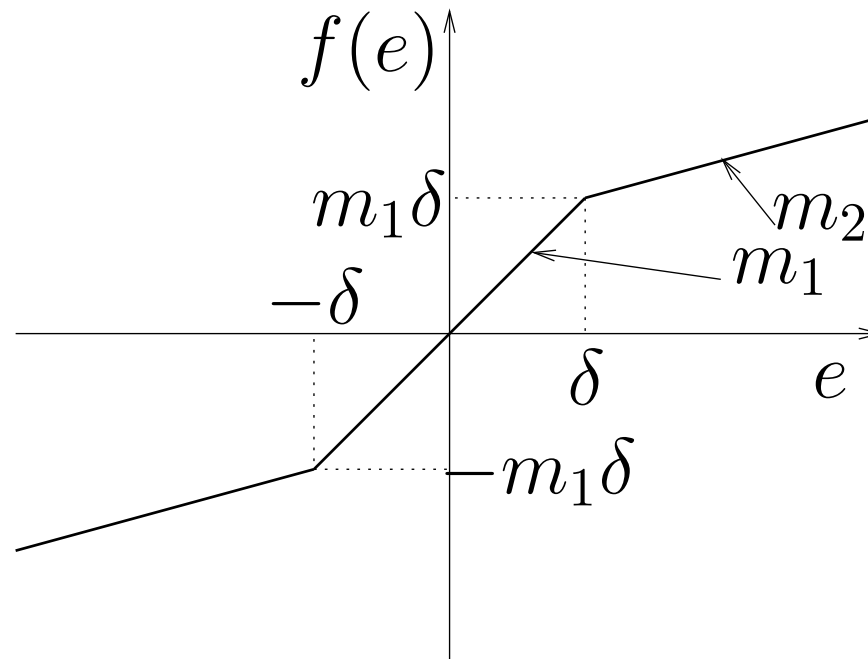
Example, $n = 3$: *(Maths Databook)*

$$(E \sin \theta)^3 = E^3 \left(\frac{3}{4} \sin \theta - \frac{1}{4} \sin(3\theta) \right)$$

so $U_1 = \frac{3E^3}{4}$, $V_1 = 0$, hence $\boxed{N(E) = \frac{3E^2}{4}}$.



Piecewise-linear non-linearity



$$f(e) = \begin{cases} m_1 e & \text{if } |e| < \delta \\ (m_1 - m_2)\delta + m_2 e & \text{if } e > \delta \\ (m_2 - m_1)\delta + m_2 e & \text{if } e < -\delta \end{cases}$$



Again $V_1 = 0$.

$$E \leq \delta: U_1 = \frac{1}{2\pi} \int_0^\pi m_1 E \sin^2 \theta d\theta = m_1 E$$

$E > \delta$:

$$U_1 = \frac{4}{\pi} \int_0^{\pi/2} f(E \sin \theta) \sin \theta d\theta,$$

$$= \frac{4}{\pi} \int_0^{\sin^{-1}(\delta/E)} m_1 E \sin^2 \theta d\theta +$$

$$\frac{4}{\pi} \int_{\sin^{-1}(\delta/E)}^{\pi/2} ((m_1 - m_2)\delta + m_2 E \sin \theta) \sin \theta d\theta$$



$$\begin{aligned}
 U_1 = & \frac{2m_1 E}{\pi} \left[\theta - \frac{1}{2} \sin(2\theta) \right]_0^{\sin^{-1}(\delta/E)} + \\
 & \frac{4(m_2 - m_1)\delta}{\pi} [\cos \theta]_{\sin^{-1}(\delta/E)}^{\pi/2} + \\
 & \frac{2m_2 E}{\pi} \left[\theta - \frac{1}{2} \sin(2\theta) \right]_{\sin^{-1}(\delta/E)}^{\pi/2}
 \end{aligned}$$



Using $\cos(\sin^{-1} x) = \sqrt{1 - x^2}$ and $\sin(2 \sin^{-1} x) = 2x\sqrt{1 - x^2}$ gives:

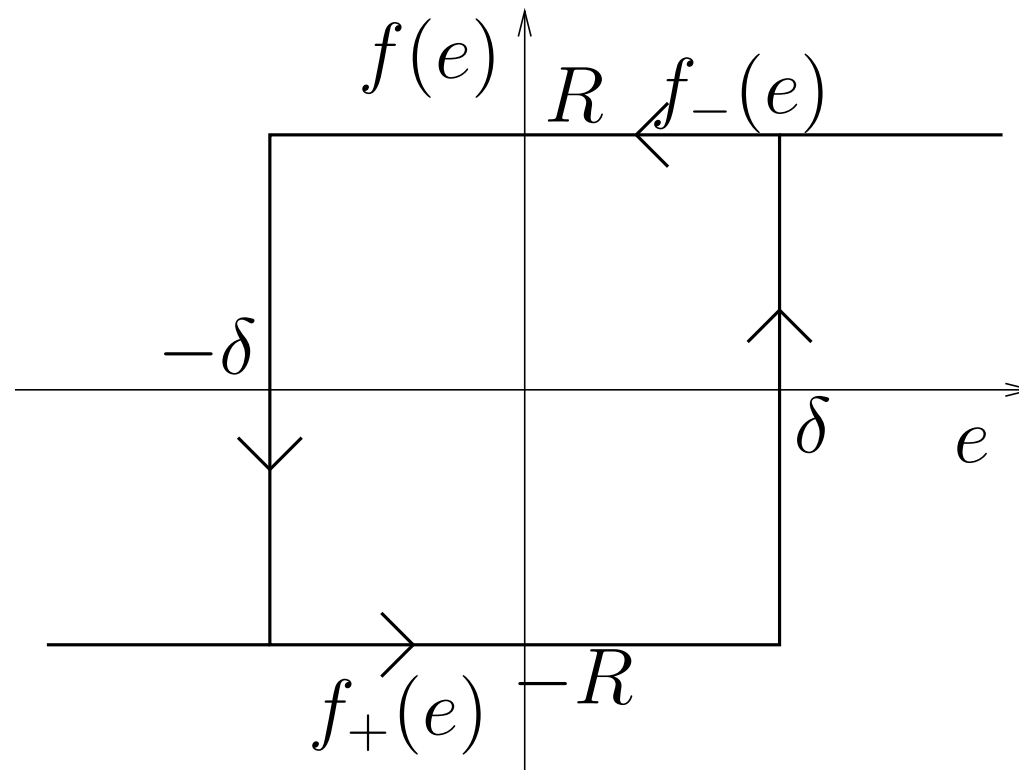
$$U_1 = \frac{2(m_1 - m_2)E}{\pi} \left[\sin^{-1}\left(\frac{\delta}{E}\right) + \frac{\delta}{E} \left(1 - \left(\frac{\delta}{E}\right)^2\right)^{1/2} \right] + m_2 E.$$

Hence

$$N(E) = \begin{cases} m_1, & \text{if } E < \delta \\ \frac{2(m_1 - m_2)}{\pi} \left[\sin^{-1}\left(\frac{\delta}{E}\right) + \frac{\delta}{E} \left(1 - \left(\frac{\delta}{E}\right)^2\right)^{1/2} \right] + m_2 & \text{if } E > \delta \end{cases}$$



Relay with hysteresis



Nonlinearity *with memory*.
Assume $E > \delta$.



$$N(E) = \frac{1}{\pi E} \int_{-\pi/2}^{3\pi/2} f(E \sin \theta) (\sin \theta + j \cos \theta) d\theta$$

Note limits of integration.

$$N(E) = \frac{1}{\pi E} \int_{-\pi/2}^{\pi/2} f_+(E \sin \theta) (\sin \theta + j \cos \theta) d\theta +$$

$$\frac{1}{\pi E} \int_{\pi/2}^{3\pi/2} f_-(E \sin \theta) (\sin \theta + j \cos \theta) d\theta$$



Real part of $N(E)$

Let $\nu = E \sin \theta$, $d\nu = E \cos \theta d\theta$.

Note $\cos \theta > 0$ if $-\pi/2 < \theta < \pi/2$,
and $\cos \theta < 0$ if $\pi/2 < \theta < 3\pi/2$.

$$\begin{aligned}\operatorname{Re} N(E) &= \frac{1}{\pi E} \int_{-E}^E f_+(\nu) \left(\frac{\nu}{E} \right) \frac{d\nu}{E \sqrt{1 - (\nu/E)^2}} \\ &\quad - \frac{1}{\pi E} \int_E^{-E} f_-(\nu) \left(\frac{\nu}{E} \right) \frac{d\nu}{E \sqrt{1 - (\nu/E)^2}} \\ &= \frac{1}{\pi E} \int_{-E}^E [f_+(\nu) + f_-(\nu)] \left(\frac{\nu}{E} \right) \frac{d\nu}{E \sqrt{1 - (\nu/E)^2}}\end{aligned}$$



Imaginary part of $N(E)$

$$\begin{aligned}\operatorname{Im} N(E) &= \frac{1}{\pi E} \int_{-E}^E f_+(\nu) \frac{d\nu}{E} + \frac{1}{\pi E} \int_E^{-E} f_-(\nu) \frac{d\nu}{E} \\ &= \frac{1}{\pi E^2} \int_{-E}^E [f_+(\nu) - f_-(\nu)] d\nu \\ &= -\frac{\Delta}{\pi E^2}\end{aligned}$$

Δ is area enclosed by the ‘loop’.



$N(E)$ for the relay

$$\begin{aligned}\operatorname{Re} N(E) &= \frac{4R}{\pi E} \int_{\delta}^E \frac{\nu d\nu}{E^2 \sqrt{1 - (\nu/E)^2}} \\ &= \frac{4R}{\pi E} \sqrt{1 - \left(\frac{\delta}{E}\right)^2}\end{aligned}$$

hence

$$N(E) = \frac{4R}{\pi E} \left(\sqrt{1 - \left(\frac{\delta}{E}\right)^2} - \frac{j\delta}{E} \right).$$



Estimates of the DF

- *Example: Piecewise-linear nonlinearity:*

$$m_2 < N(E) \leq m_1$$



Estimates of the DF

- *Example: Piecewise-linear nonlinearity:*

$$m_2 < N(E) \leq m_1$$

- *Example: Relay with dead-zone:*

$$f(e) = \begin{cases} -1, & \text{if } e \leq -\delta \\ 0, & \text{if } |e| < \delta \\ +1, & \text{if } e \geq \delta \end{cases}$$

$N(E)$ increases rapidly for $|e|$ just above δ , then falls towards 0.

