

Tracking beyond the Nyquist frequency in sampled-data systems

- going beyond the sampling limit

Dedicated to Malcolm Smith
on the occasion of his 60th birthday

Yutaka Yamamoto
Kyoto University, Emeritus
CentraleSupélec

Our encounters

- Many conferences
- 1997, few days visit to Cambridge



Malcolm playing piano at my home,
after CDC 1996 Kobe



Control 2000



MTNS 2006



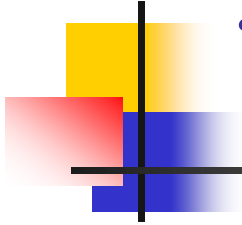
Joint work with



Kaoru Yamamoto,
Lund University

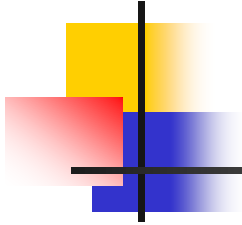


Masaaki Nagahara,
U. Kitakyshu

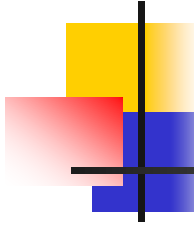


Topic of this talk

- Tracking to signals beyond the Nyquist frequency



WHAT'S SO SPECIAL
ABOUT IT?



Claude Shannon



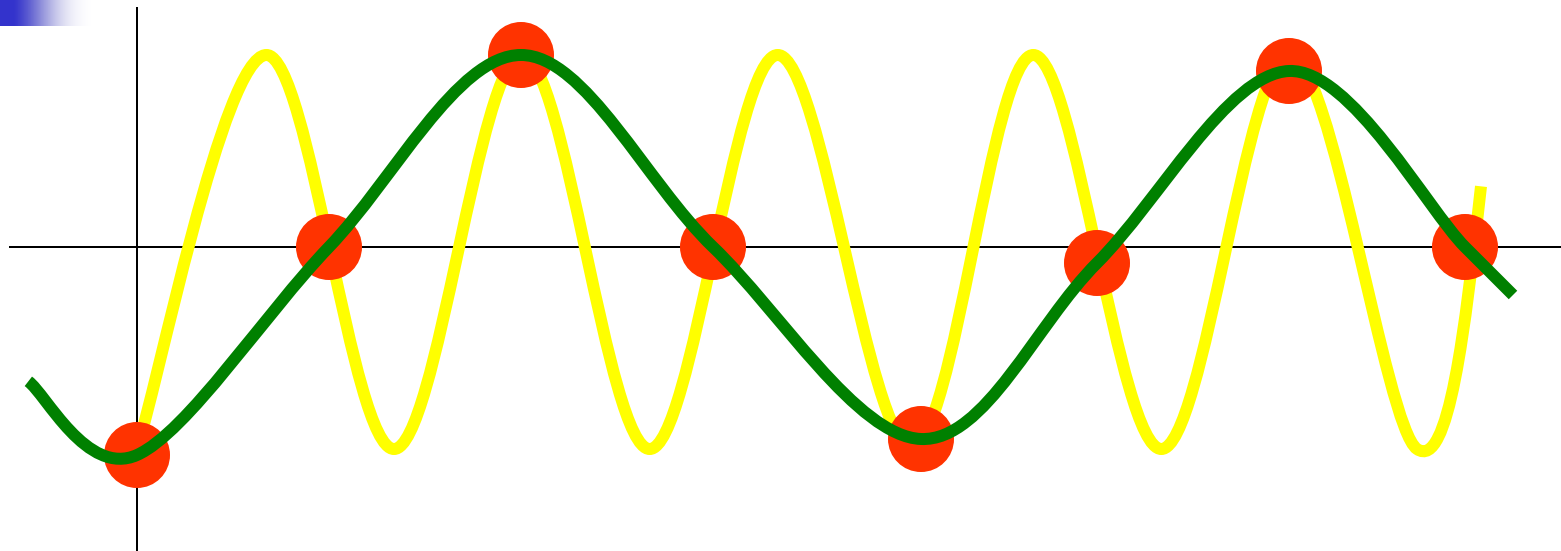
- Communication in the Presence of Noise, C. E. Shannon, Proc. IRE, vol. 37, 1949, pp. 10–21.
- *How fast should we sample in transmitting data through a channel?*
- $\Rightarrow$ *Unique reconstruction below the Nyquist frequency*

Claude Elwood Shannon (1916–2001)

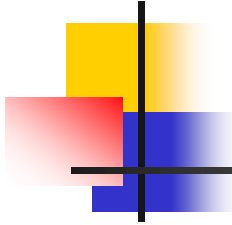
July 5, 2017

Typical difficulty

Sampling $\rightarrow$ Aliasing

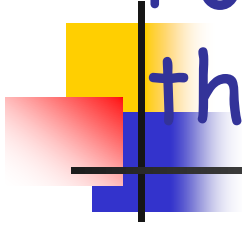


- High-freq. intersample information can be lost
- If no high-freq. components beyond the **Nyquist frequency** ($=1/2$ of sampling freq.) $\rightarrow$ unique restoration
 - $\rightarrow$ Whittaker-Shannon-Someya sampling theorem



Observation

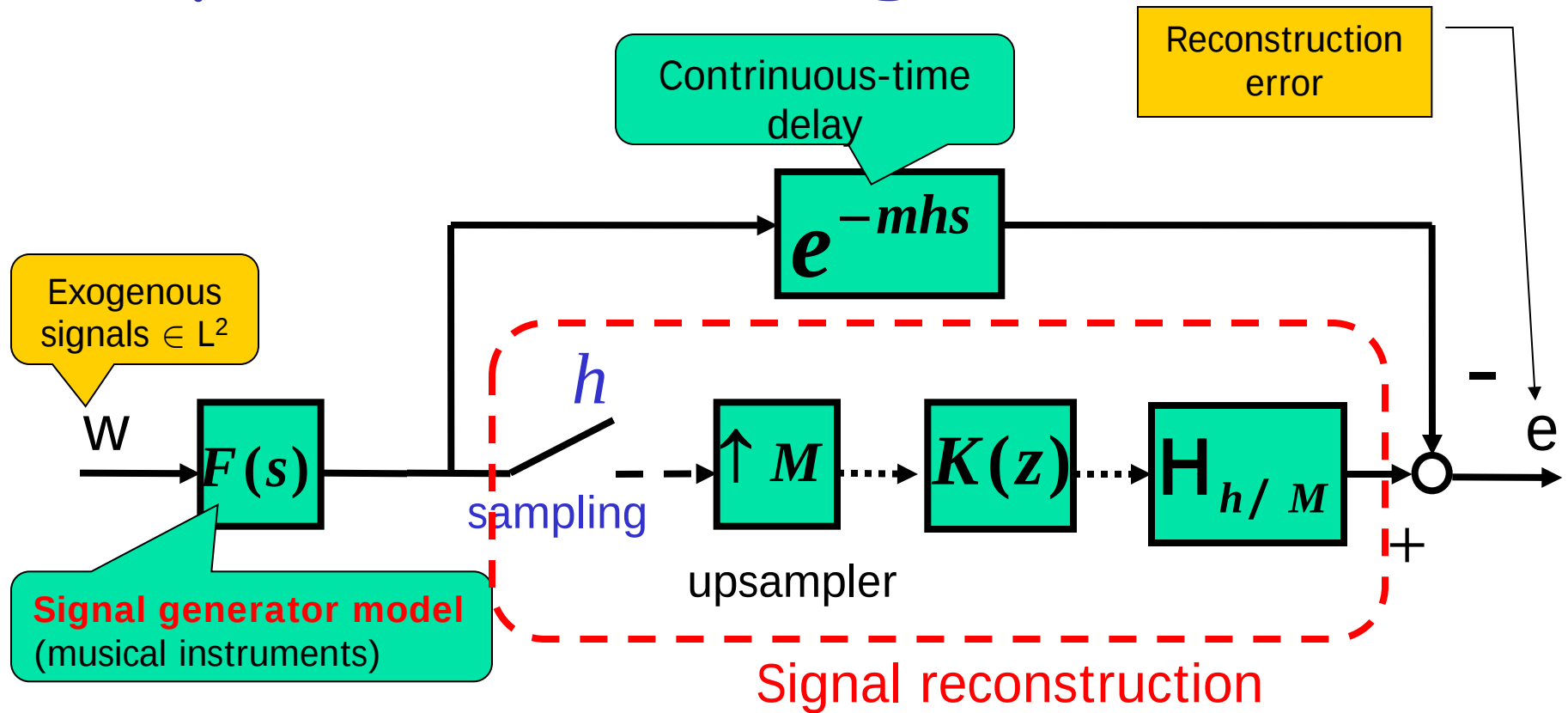
- Low and high frequencies cannot be distinguished.
- $\Rightarrow$ truncate high frequency and concentrate on low frequency
- Bound = π/h , Nyquist frequency
- This “Shannon paradigm” has been prevalent for the past 60+ years



Popular (but wrong) understanding of the Shannon paradigm

- *We can do nothing for signals beyond the Nyquist frequency*
- **This is wrong**
- Hidden assumption: no information on high-freq. $\Rightarrow$ Band limiting hypothesis

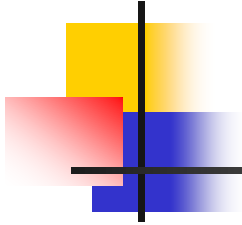
Sampled-data Design Model



Problem: Find $K[z]$ satisfying

$$\|T_{ew}\| < \gamma$$

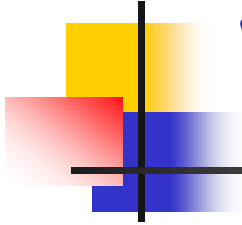
Sampled-data H^∞ control problem



Moving image demo

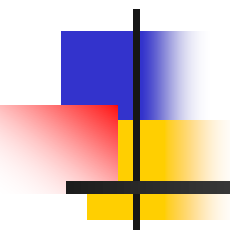


Left: Bicubic - no high freq. beyond Nyquist freq
Right: yy (reconstructed high freq.)

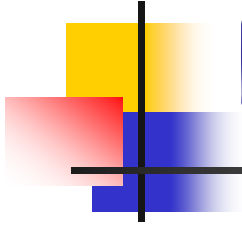


Why success?

- Signal generator model $F(s)$
- This contains information on high frequency
- Allows us to recover high freq. components

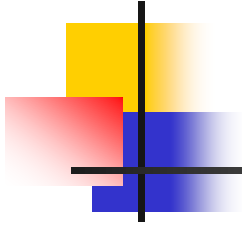


New question



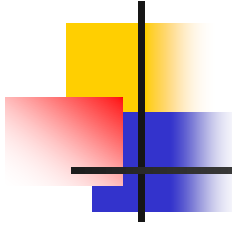
Can we control signals beyond the Nyquist freq.?

- Dates back to an old question in 1993
- “*Can we control high-freq. through aliases?*”



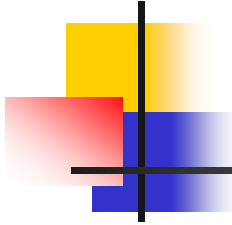
Demands

- Hard disk drives
- Often high-freq. disturbances (due to winds)
- Sampling frequency is limited by a physical limitation
- Can we reject such high-freq. disturbances? (beyond the Nyquist frequency)



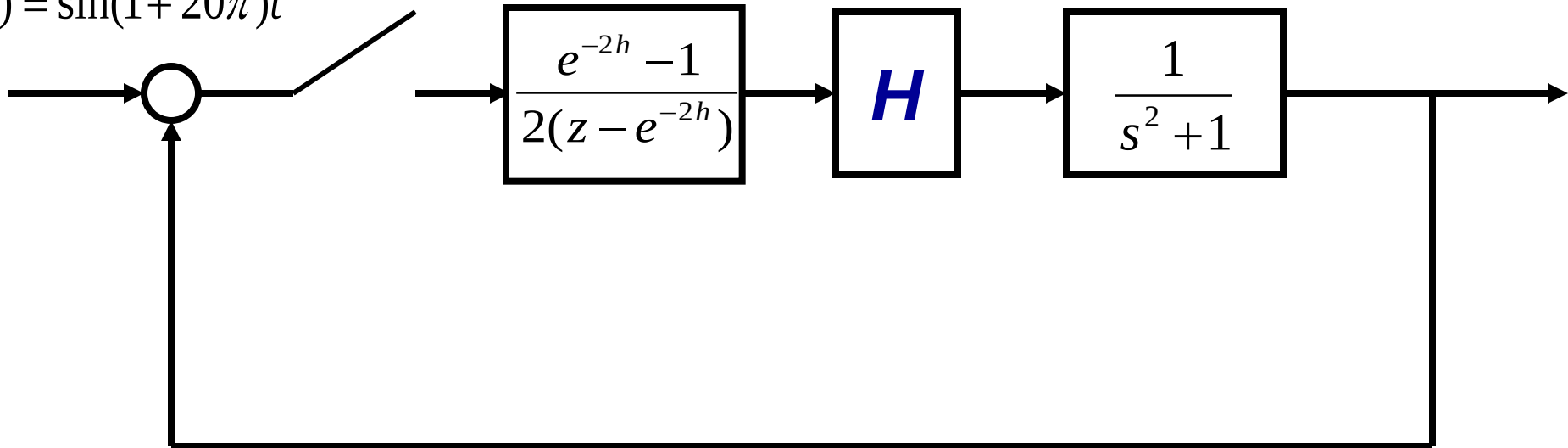
1st Tracking Problem

- Sampled-data system
- Sampling period h
- Nyquist frequency: π/h [rad/sec]
- Can we track a reference with frequency higher than π/h ?



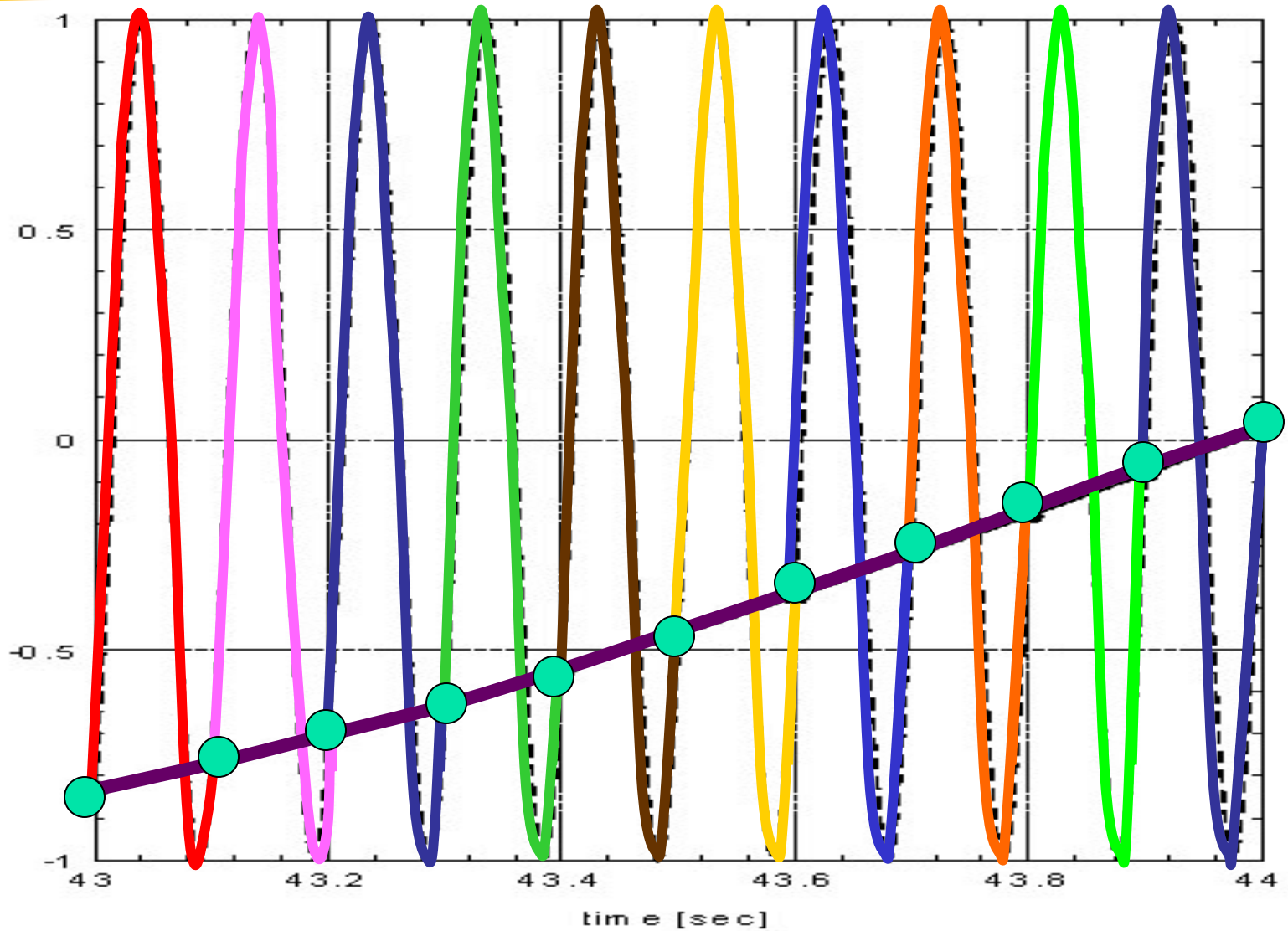
Counterexample?

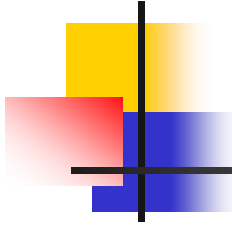
$$r(t) = \sin(1 + 20\pi)t$$



Response

$$v(\theta) = \sin(1 + 20\pi)\theta$$

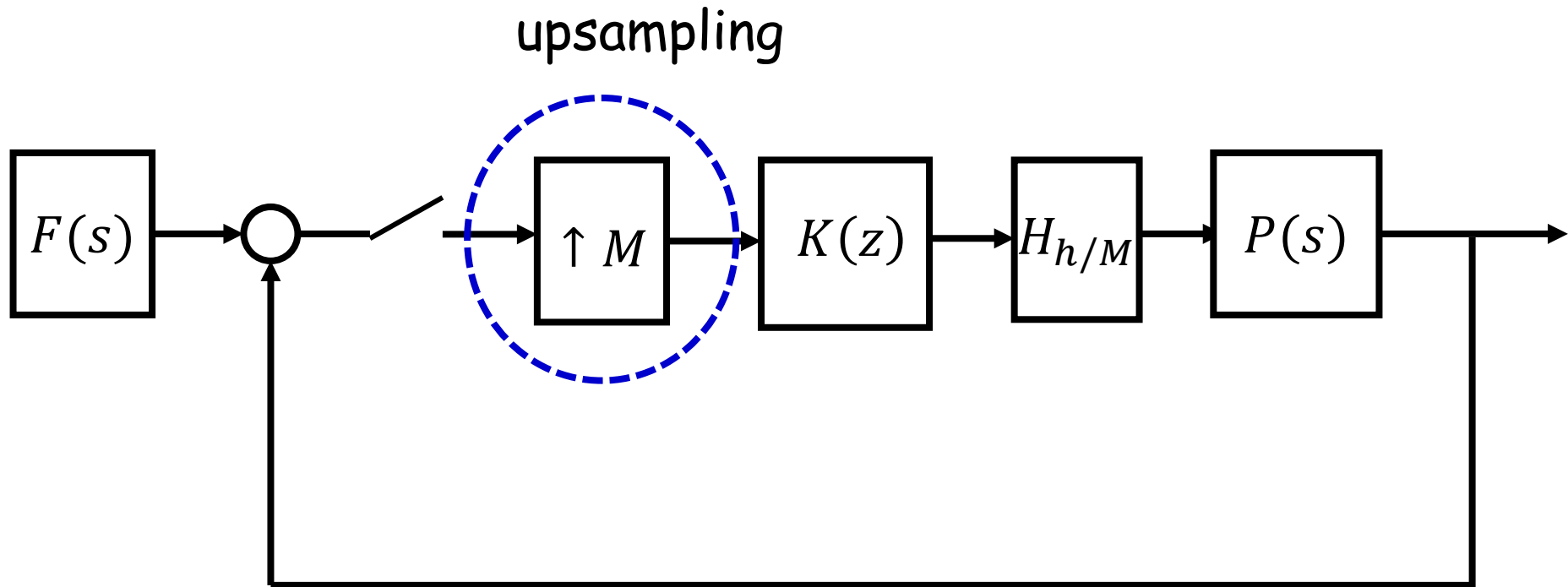


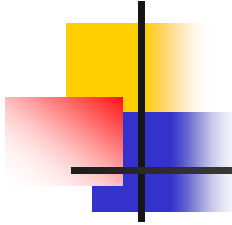


Recipe

- We need **upsampling** to take care of the intersampling behavior
- We need a **proper weighting** in the high frequency range (i.e., right signal model)

Basic construction

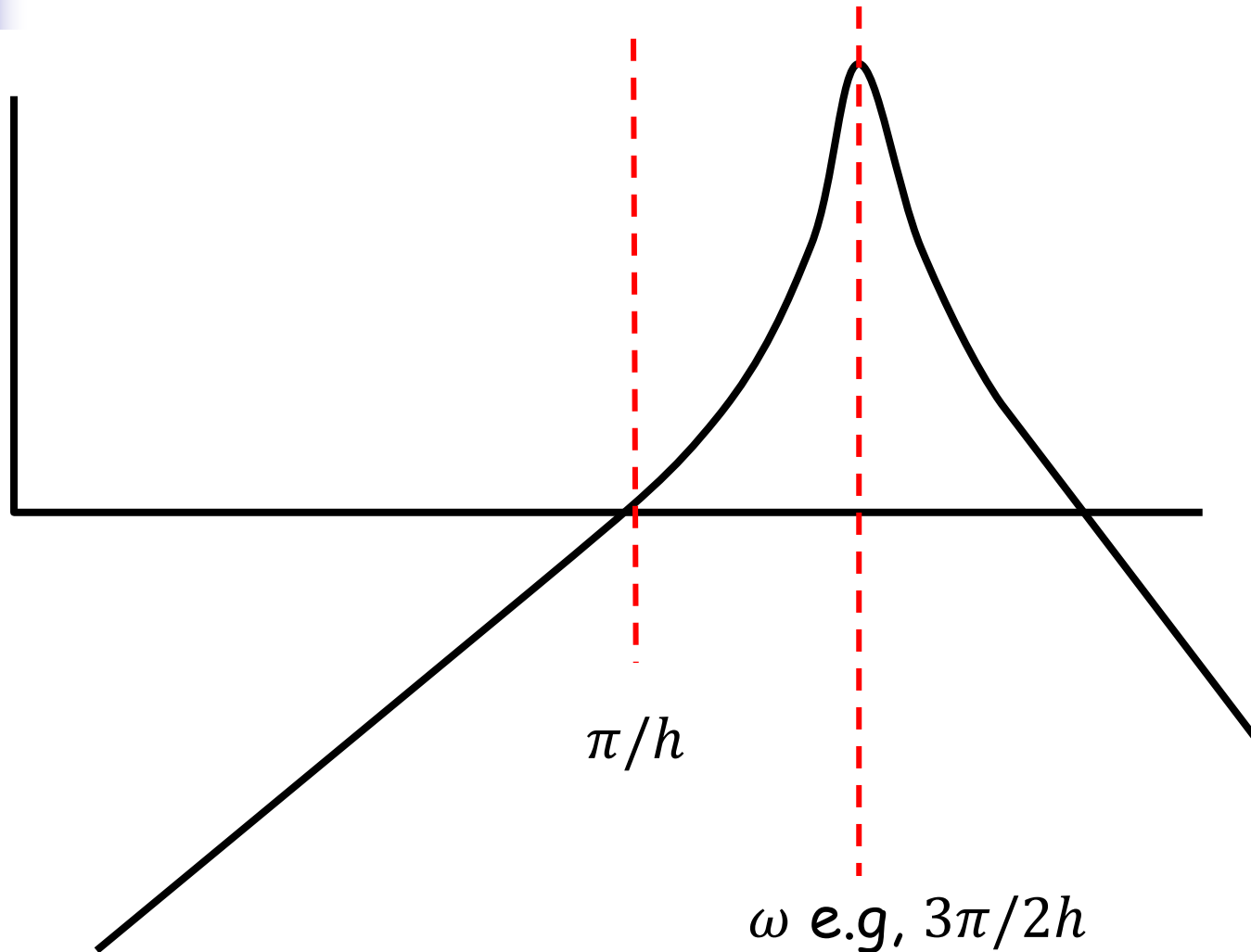




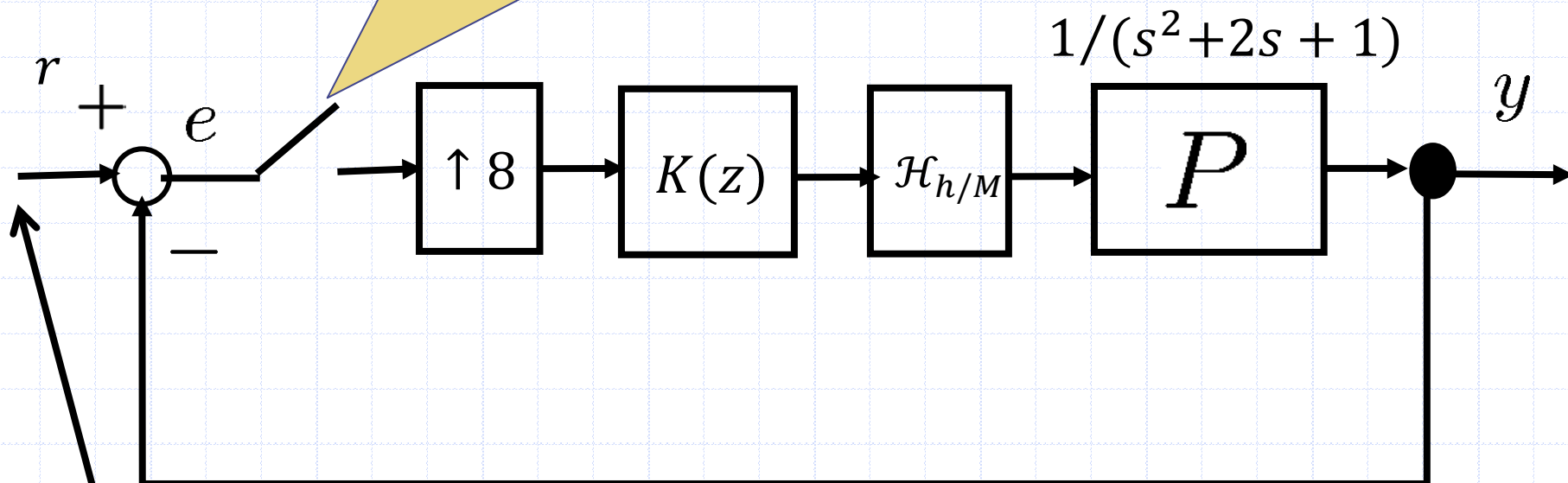
Example

- $P(s) = \frac{1}{s^2 + 2s + 1}$
- $h = 1$, Nyquist freq. $= \pi$
- $r(t) = (3\pi/2)t$
- $F(s) = \frac{s}{s^2 + 0.1s + (3\pi/2)^2}$, peak at $(3\pi/2)$

signal model $F(s)$



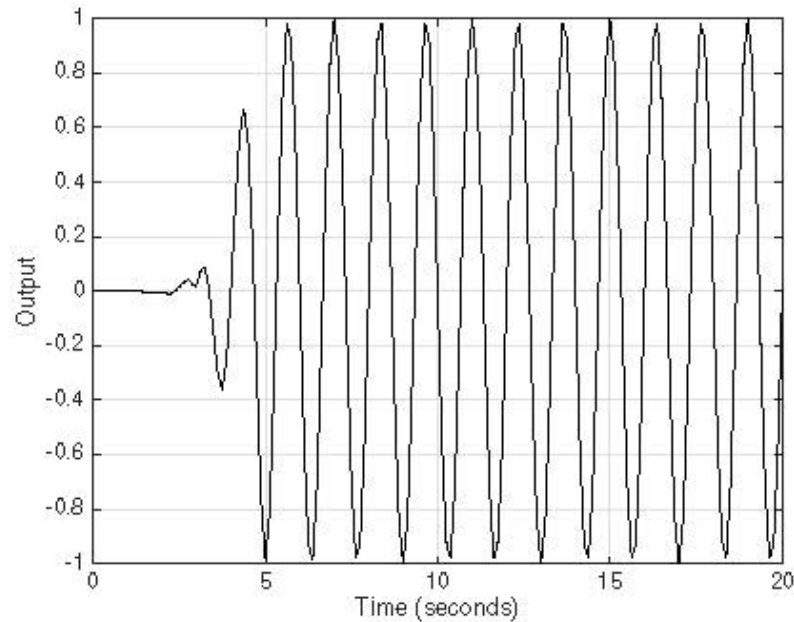
Slow sampling; only low
freq. signals can be detected



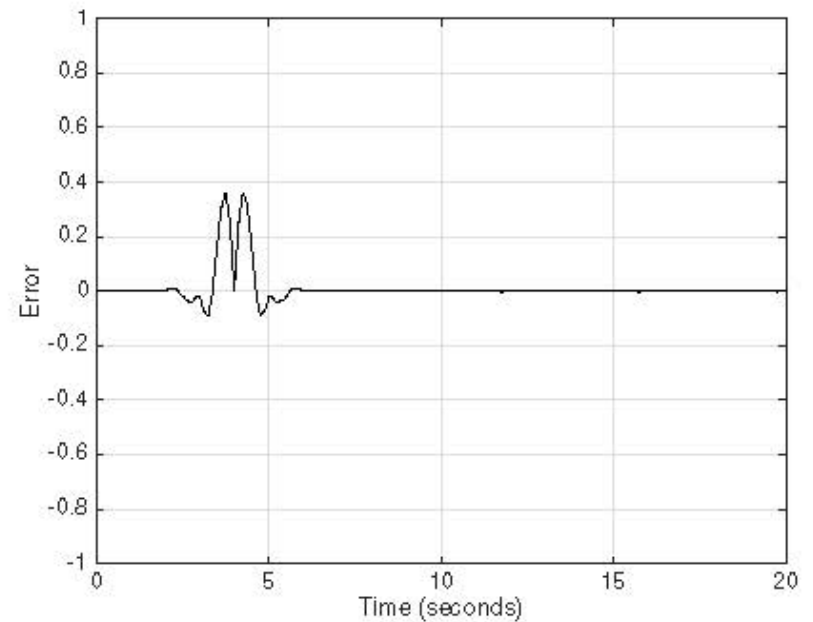
$$\frac{s}{s^2 + 0.1s + (3\pi/2)^2}$$

weight

Example - results



$y(t)$

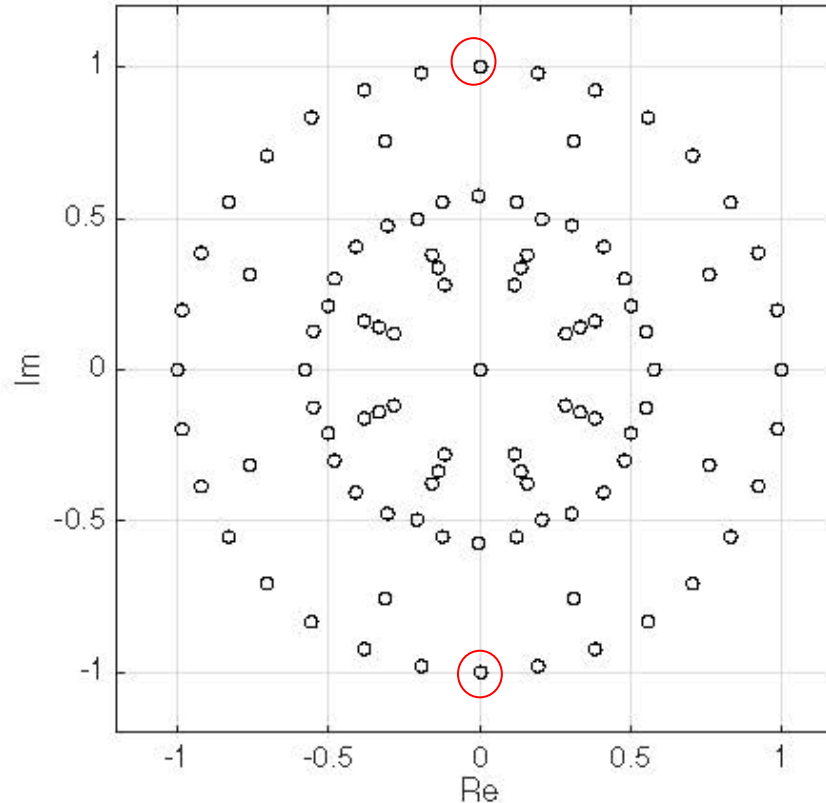


$e(t)$

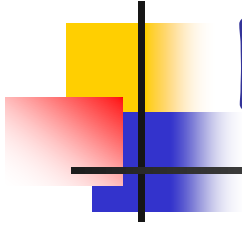
Presented at the
CDC 2016, Las Vegas

Poles in the controller

This gives rise to an **approx. internal model** along with the upsampler+fast hold

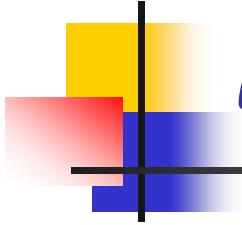


Poles at $e^{\pm j(3/2\pi)} = \pm j$.



Next questions

- Disturbance rejection
- More than one reference or disturbance signals?
- robustness

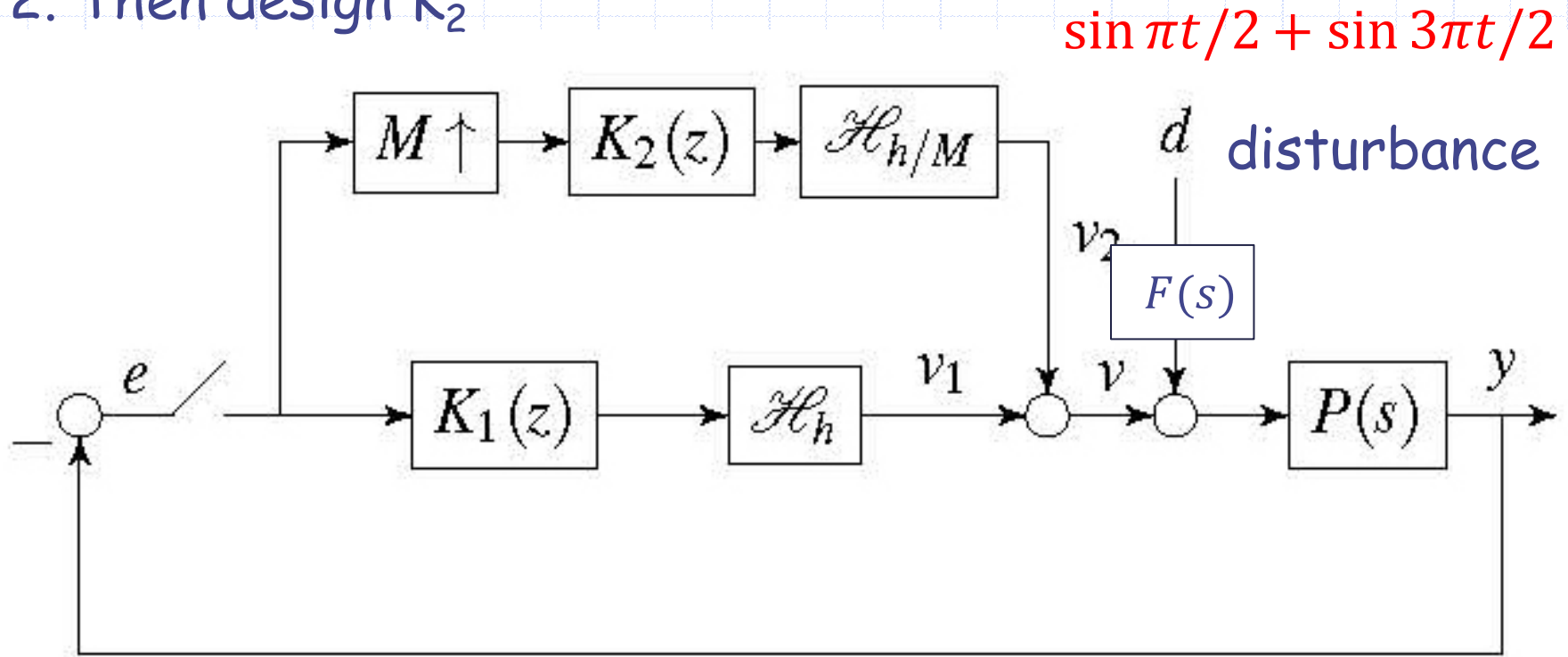


More than one signals

- Standard recipe: weights at two frequencies
 - May work, but
- Fails if they are separated by π
- Sampling cannot distinguish two signals

Two step design:

1. Design K_1 for low frequency
2. Then design K_2



Two step design configuration

$$F(s) = \frac{50s}{(s^2 + 0.2s + \omega_1^2)(s^2 + 0.1s + \omega_2^2)}$$

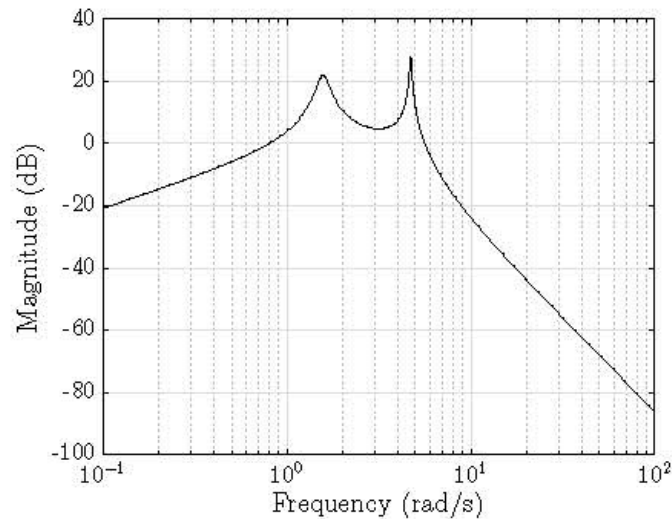


Fig. 4. Weighting function $F(s)$.

Weighting function

To be presented at the
1st IEEE CCTA, Hawaii,
2017

Output $y(t)$

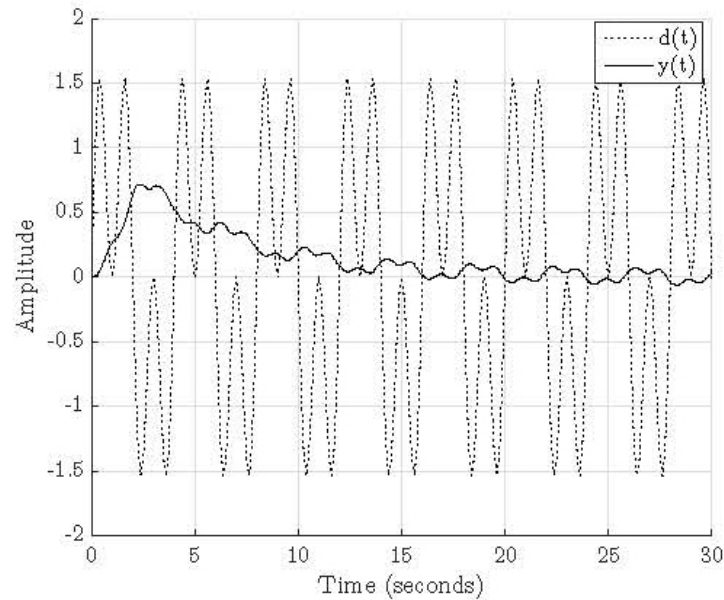
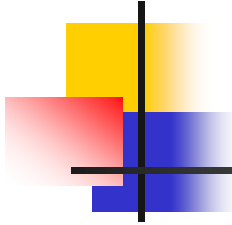


Fig. 8. System output (solid) against disturbance $\sin(\pi/2)t + \sin(3\pi/2)t$ (dotted).



Conclusion

- Tracking/rejection are possible for signals beyond the Nyquist frequency
- Not limited by the Shannon paradigm
- Crucial elements:
 - a. Physical model
 - b. appropriate weighting
 - c. upsampling (multirate processing)
- Many more applications expected

Happy 60th Malcolm!



YY Fest 2010

**Symposium on Systems, Control,
and Signal Processing
In honor of Yutaka Yamamoto
on the occasion of his 60-th birthday**



At YYFest 2010



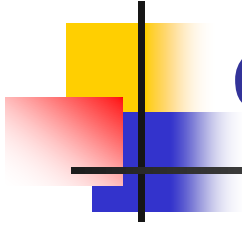
YYFest, 2010





MTNS 2006, Kyoto





I want to thank you for yet another:

- Malcolm was Kaoru's Ph. D. supervisor for 2011-2015
- Kaoru got a Ph. D. under his supervision
- Thesis title: "Disturbance Attenuation in Mass Chains with Passive Interconnection"

At the graduation ceremony at Caius



April, 2016



Thank you Malcolm for your
Long-term friendship,
Superb supervision of Kaoru,
Many happy returns
Of the day!